MID-TERM EXAM GEOPHYSICAL FLUID DYNAMICS 10 November 2010, 9.00 - 11.00 hours Two problems (all items have equal weight)

Remark: answers may be written in English or Dutch.

Problem 1

Consider a fluid that is bounded from below by a fixed level z = b and from above by a free level $z = \eta$.

One of the equations governing the dynamics of this fluid is

$$\frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} - f u = -g \frac{\partial \eta}{\partial y} \tag{(*)}$$

- a. Name, define and describe the physical meaning of parameter f. Also, name the variables that appear in the equation f.
- b. Is this flow characterised by a small Richardson number?
 Explain your answer by defining this number and explaining its physical meaning.
- c. Name the first term on the right-hand side of Eq. (*) and derive it from a term that occurs in the equations of motion for a molecular viscous fluid.

Assume that the flow is steady, that $\partial b/\partial x = 0$ and that $\partial b/\partial y = 0.02$. Furthermore, it is given that in point P, which is at location x = 0, y = 0 and halfway the fluid column, velocity $v = 1 \text{ m s}^{-1}$ and velocity $w = 0.05 \text{ m s}^{-1}$ (see figure).

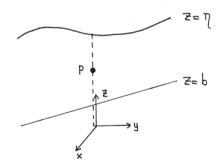


Figure 1: Situation sketch. The *x*-axis points out of the paper.

- d. Compute at this x, y-location the values of v and w at the bottom. Explain how you obtain your answer.
- e. Compute at this x, y-location the values of v and w at the free surface. Explain how you obtain your answer.

For problem 2: P.T.O.

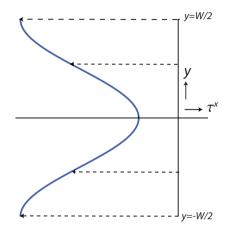
Problem 2

In an area north of the equator the wind stress over the surface of the ocean is given by

$$\tau^x = -T_0 + \hat{T} \cos\left(\frac{2\pi y}{W}\right), \qquad \tau^y = 0.$$

Here, $-W/2 \le y \le W/2$ and $0 < \hat{T} < T_0$ (see figure).

This winds stress generates steady and linear large-scale flow that is uniform in the zonal direction. Furthermore, assume parameters f and ν_E to be constants.



- a. Assuming that there is no geostrophic flow in the interior of the ocean (the ocean is infinitely deep), sketch the velocity vector (with components u and v) in the ocean as a function of vertical coordinate z at location y = 0. Explain your answer.
- b. Compute the transports U and V at y = 0 in terms of parameters f, T_0, \hat{T} and W. Hint: integrate the momentum equations.
- c. Compute and sketch the distribution of the surface Ekman pumping velocity as a function of y. Also, give a short interpretation of your result.

Assume now that the ocean has a finite depth and that the Ekman pumping near the bottom is identical to that induced by the surface Ekman layer.

- d. Sketch the resulting pressure distribution in the ocean and the transport distribution in the bottom Ekman layer.
- e. Compute the geostrophic flow in the interior of the ocean, assuming that its areaaveraged value is zero.
- f. Derive an expression for the (relative) circulation in the interior of the ocean in the domain defined by $0 \le x \le L$ and $0 \le y \le W/2$. Here, L is a fixed length.

END

Continuity and momentum equations: molecular viscous fluid

$$\begin{aligned} \frac{\partial \rho}{\partial t} &+ \frac{\partial}{\partial x} (\rho \, u) \,+ \, \frac{\partial}{\partial y} (\rho \, v) \,+ \, \frac{\partial}{\partial z} (\rho \, w) \,= \, 0 \\ \rho \left(\frac{du}{dt} \,+ \, f_* \, w \,- \, f \, v \right) &= \, - \, \frac{\partial p}{\partial x} &+ \mu \left(\frac{\partial^2 u}{\partial x^2} \,+ \, \frac{\partial^2 u}{\partial y^2} \,+ \, \frac{\partial^2 u}{\partial z^2} \right) \\ \rho \left(\frac{dv}{dt} \,+ \, f \, u \right) &= \, - \, \frac{\partial p}{\partial y} &+ \mu \left(\frac{\partial^2 v}{\partial x^2} \,+ \, \frac{\partial^2 v}{\partial y^2} \,+ \, \frac{\partial^2 v}{\partial z^2} \right) \\ \rho \left(\frac{dw}{dt} \,- \, f_* \, u \right) &= \, - \, \frac{\partial p}{\partial z} \,- \, \rho g &+ \mu \left(\frac{\partial^2 w}{\partial x^2} \,+ \, \frac{\partial^2 w}{\partial y^2} \,+ \, \frac{\partial^2 w}{\partial z^2} \right) \end{aligned}$$

Energy budget for adiabatic flow of fixed composition

$$\rho C_v \frac{dT}{dt} - \frac{T}{\rho} \left(\frac{\partial p}{\partial T}\right)_\rho \frac{d\rho}{dt} = 0$$

Relative circulation and relative vorticity

$$\Gamma = \oint_C \mathbf{u} \cdot d\mathbf{r} = \int_S (\nabla \times \mathbf{u}) \cdot \mathbf{n} \, dS$$

where S is the surface enclosed by contour C.

Shallow water equations

$$\begin{aligned} \frac{\partial u}{\partial t} &+ u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} - f v &= -g \frac{\partial \eta}{\partial x} \\ \frac{\partial v}{\partial t} &+ u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + f u &= -g \frac{\partial \eta}{\partial y} \\ \frac{\partial \eta}{\partial t} &+ \frac{\partial}{\partial x} (hu) + \frac{\partial}{\partial y} (hv) &= 0 \end{aligned}$$

Ekman pump (Northern Hemisphere)

$$\overline{w} = \frac{d}{2}\overline{\zeta}, \qquad d = \left(\frac{2\nu_E}{f}\right)^{1/2} \quad \text{and} \quad w_{Ek} = \frac{1}{\rho_0 f} \left[\frac{\partial \tau^y}{\partial x} - \frac{\partial \tau^x}{\partial y}\right]$$